«Calculation of the effective separation of light impurities in the inertial jalousie-countercurrent dust collector»

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Gamma-shaped inertial jalousie-countercurrent dust collector

1, 5 – inlet and outlet pipes of the dust collector; 2, 4 – initial and final sections of the jalousie grate; 6 – dividing wall; 7 – dust-settling chamber; 8 – sluice valve; 9, 11 – outlet pipes of jalousie separator and countercurrent separator; 10 – adjacent wall of outlet pipes of separators

\[ L = l_1 + l_2 \]

- \[ \rightarrow \] – air with light impurities
- \[ a \rightarrow \] – purified air
- \[ \rightarrow \rightarrow \] – separated light impurities
G. Yu. Stepanov, I. M. Zicer in the book «Inertia air cleaners» gave recommendations for the calculation of the constructive-technological parameters of the inertial jalousie dust collectors. For example, an algorithm for calculating the jalousie separator is given and the following parameters of the jalousie grating are recommended: the angle of inclination of the front surface of the grating to the direction of air flow \( \alpha = 6...7^\circ \); the angle of inclination of the plates in the jalousie grating \( \beta = 25...30^\circ \); the step \( S \) of the plates should be taken as minimum possible; the length \( l \) of the plates is equal to the step \( S \) at the recommended \( \alpha \) and \( \beta \); the average air velocity at the inlet to the dust collector should be \( V_o = 9...15 \) m/s.

The suction coefficient \( q \) equal to the ratio of the amount of air \( Q_1 \) which is withdrawn together with the separated dust to the amount of air \( Q_j \) which passed through the jalousie grate should be values

\[
q = Q_1 / Q_j = 0,1...0,2.
\]  
(1)

The effect of the release of light impurities by the jalousie dust collector (\%) from the removed air is determined by the formula

\[
E_j = \left( \frac{q}{1+q} \right)^{\varepsilon_01} \cdot 100,
\]  
(2)

where \( \varepsilon_01 \) – the dust transmission coefficient for one channel of the jalousie grating (in fractions from one) with characterized the amount of separated dust to its total amount and can be calculated on a computer using the described algorithm.
The parameters of the inertial jalousie-countercurrent dust collector are the height $H_o$, the area $F_o$ of the cross section of the inlet pipe, the length $L$ and the area $F$ of the surface of the jalousie grate, the height $H$ of the dust collector, the heights $h_j$, $h_c$ and the areas $F_1$, $F_2$ of the cross sections of the output holes of the jalousie separator and countercurrent separator, the angle $\gamma$, which determines the position of the dividing wall 6 relative to the horizontal passing through the lower edge of the adjacent wall 10.

The height $H_o$ (m) is determined by the total air flow $Q_o$ (m$^3$/s) passing through the dust collector and the air inlet velocity $V_o$:

$$H_o = \frac{Q_o}{B \cdot V_o},$$

(3)

where $B$ – the width of the dust collector equal to the width of the air system of the grain cleaning machine, m.

The suction coefficient at the same width $B$ in the dust collector and the jalousie grate is equal to:

$$q = \frac{Q_1}{Q_j} = \frac{V_1 \cdot h_j}{V' \cdot b' \cdot z},$$

(4)

where $V_1$, $V'$ – the average air velocity in the outlet of the jalousie separator and the air jet passing between the plates of the jalousie, m/s;

$b'$ – the height of the air jet passing between the plates, m;

$z$ – number of channels in the grate.
Since the number of channels \( z \) and the length of the jalousie grate \( L \) (m) are determined by the formulas:

\[
L = \frac{H_o - h_J}{\sin \alpha}, \quad z = \frac{L}{S}.
\]  

(5)

For "dense jalousie grate" [4], when \( S \leq l \), the expressions are valid

\[
\frac{V'}{V_1} = \frac{\sin(\alpha + \beta/2)}{\sin (\beta/2)}; \\
\frac{b'}{S} = \frac{\sin \alpha \cdot \sin \beta}{\sin \alpha + \sin(\alpha + \beta)}; \\
\]

(6)  

(7)  

then is the height of the outlet of jalousie separator

\[
h_J = \frac{H_o}{1 + \frac{\sin(\beta/2) \cdot [\sin \alpha + \sin(\alpha + \beta)]}{q \cdot \sin(\alpha + \beta/2) \cdot \sin \beta}}.
\]  

(8)

It should be taken into account that the expression (8) is derived without taking into account the influence of the countercurrent separator and is therefore approximate.

To estimate the impact of the design and technological parameters of the countercurrent separator on the efficiency of its operation we will use a simplified air flow model that takes into account the basic laws of the real process.
The air jet at the flow rotation is modeled by a ring with internal $R_1$ and external $R_2$ radiiuses.

Then the height $h_c$ of the outlet of the countercurrent separator is determined by the radius $R_1$ of the turn of the annular jet:

$$h_c = h_j + 2 \cdot R_1 .$$

(9)

The radiiuses $R_1$ and $R_2$ of the jet boundaries are determined from the continuity condition of the flow:

$$B \cdot h_j \cdot V_1 = \int_{R_2}^{R_2} B \cdot V_{2i} \cdot dr ,$$

(10)

where $V_{2i}$ – the flowing air velocity in the $i$-section of the annular jet, m/s.

When the jet is rotated the air velocity depends on the radial coordinate $r_i$ and changes according to the law of the potential circular flow

$$V_{2i} = V_{2\text{max}} \cdot \frac{R_1}{r_i} ,$$

(11)

where $V_{2\text{max}}$ – the air velocity at the inner boundary of the jet, m/s.
According to the research of I. E. Idelchik [7] when the air jet turns 180° near the edge of a continuous adjacent wall the expression is rightly:

\[
\left( \frac{V_{2,\text{max}}}{V_2} \right)^2 = 4, \tag{12}
\]

where \( V_2 \) – the average air velocity in the annular jet of the separator, m/s.

\[
h_j = (R_2 - R_1) \cdot \cos \gamma ; \tag{13}
\]

\[
\psi_{\text{max}} = \pi \pm \gamma , \tag{14}
\]

From the condition of continuity of the annular jet

\[
V_1 = V_2 . \tag{15}
\]

\[
h_j = 2 \cdot R_1 \cdot \ln \frac{R_2}{R_1} . \tag{16}
\]

\[
R_2 = R_1 \cdot \exp \frac{h_j}{2 \cdot R_1} . \tag{17}
\]

Then the turning radius of the jet is equal to

\[
R_1 = \frac{h_j}{[\exp(h_j/2 \cdot R_1) - 1] \cdot \cos \gamma} . \tag{18}
\]

This equation is solved by iteration method.
The depth of the dust-reducing chamber $H$ is determined using the theory of G. N. Abramovich on a turbulent jet that gets into a dead end. According to this theory the value of the air velocity on the axis of the jet equal to 3...5% of its initial value is at a distance.

$$x = 6 \cdot (h_j + h_c). \quad (19)$$

Then the height of the dust chamber, taking into account the diameter of the sluice gate $d_{SG}$ will be the value

$$H = 6 \cdot (h_j + h_c) + d_{SG}. \quad (20)$$

The velocity at the outlet of the jalousie separator $V_1$ necessary to determine the efficiency of the countercurrent separator determined from the condition of continuity of the flow:

$$Q_O = Q_1 + Q_J. \quad (21)$$

$$V_O \cdot F_O = V_1 \cdot F_1 + V' \cdot B \cdot b' \cdot z. \quad (22)$$

When the width of the jalousie separator and dust collector is rightly the expression

$$V_O \cdot H_O = V_1 \cdot h_j + V' \cdot b' \cdot L / S. \quad (23)$$

Given the formulas (6), (7) and (23), we obtain:

$$V_1 = \frac{V_O \cdot H_O}{h_j + L \cdot \frac{\sin(\alpha + \beta/2) \cdot \sin \alpha \cdot \sin \beta}{\sin(\beta/2) \cdot [\sin \alpha + \sin(\alpha + \beta)]}}. \quad (24)$$
The trajectories of the grain dust particles which are necessary for calculating the efficiency of the countercurrent separator are determined in polar coordinates: $r_i$ – the radius where the particle is located and $\psi_i$ – the angle of rotation of the particle.

The deposition of particles of light impurities in the dust-settling chamber is determined from the following considerations. If according to the results of calculations the particle has reached the radius $R_2$ and the angle $\psi_i < \psi_{max}$, then we believe that this particle further moves by inertia and settles in the dust chamber.

The calculation of the trajectory of the particle with a diameter $\delta_i$ produce, given the values of the initial coordinate $r_i$ starting from $R_1$ until at a certain coordinate $r_B$ particle is not released from the flowing air. Assuming that the particles of this diameter $\delta_i$ are uniformly distributed in the flowing air, we determine the dust transmission coefficient by the formula

$$
\varepsilon_{ci} = \frac{r_B - R_1}{h_j}.
$$

(25)

Calculation of the coefficients of dust passing $\varepsilon_c = f(\delta)$ through a countercurrent separator depending of the particle size $\delta_i$ produced using computer algorithm G. Ju. Stepanov, I. M. Zicer for the jalousie separator with the following changes:

- the dust separation conditions in the countercurrent separator differ from those given there so the formulas (13), (14) and (17) are used to determine the radiuses $R_1, R_2$ and the angle $\psi_{max}$;
- the calculating velocity of the flowing air $V_{2i}$ over the cross section of the annular jet is used the formula (11);
- the determining average flowing air velocity at the inlet to the countercurrent separator $V_1$ the formula (24) is applied.
The coefficients of passing dust through a countercurrent separator \( \varepsilon_c \) from the size of particles \( \delta_i \) (micrometers): 1 – \( h_j = 0.02 \) m; 2 – \( h_j = 0.04 \) m; 3 – \( h_j = 0.06 \) m; 
\(--\) \( \psi_{\text{max}} = 160^\circ \); \( \cdots \cdots \cdots \) \( \psi_{\text{max}} = 170^\circ \); \(--\) \( \psi_{\text{max}} = 180^\circ \); \(-\cdot\cdot\cdot\) \( \psi_{\text{max}} = 190^\circ \); 
\(--\times\times\cdots\) \( \psi_{\text{max}} = 200^\circ \)

The effectiveness of the capture of light impurities by the countercurrent separator is improved with a decrease of the heights \( h_j \) and \( h_c \), the lower edge of the separation partition 6 should be approximately at the same level with the edge of the outlet of the jalousie separator relative to the horizontal (angle \( \gamma = 0^\circ \)). At the same time reducing the height of \( h_j \) reduces the effectiveness of the capture of light impurities by the jalousie separator.
Ignoring the change in the fractional composition of the particles during the separation of impurities in the jalousie separator we obtain a formula for determining the effect capture of light impurities (%) from the exhaust air by an inertial jalousie-countercurrent dust collector as a whole:

\[
E_o = \left( \frac{q}{1+q} \right)^{\varepsilon_{01}} \cdot \left( 100 - \int_{\delta_{\text{min}}}^{\delta_{\text{max}}} \varepsilon_{Ci} \cdot P(\delta) \cdot d\delta \right).
\]

(26)

where \( P(\delta) \) – is the particle size distribution density of light impurities.

It is installed \( \Gamma \)-shaped inertial jalousie-countercurrent dust collector with constructional parameters \( H_o = 0.16 \) m, \( \alpha = 7^\circ \), \( \theta = 30^\circ \), \( h_j = 0.04 \) m, \( h_c = 0.04 \) m, \( L = 1.0 \) m, \( H = 0.6 \) m in the air system of seed cleaning machine that functioned on the cleaning of barley seeds of Abava variety. The effect of capture of light impurities from the exhaust air in the pneumatic system as a whole was an average value \( E_o = 98.9\% \).

The developed methodology allows the determining effect of light impurities separation from the exhaust air by the \( \Gamma \)-shaped inertial jalousie-countercurrent dust collector quite accurately depending on its design parameters and fractional composition of grain dust particles.
Conclusion

It is developed a Г-shaped inertial dust collector with a flat and parallel movement of air in it, which contains alternately located of jalousie separator and countercurrent separator for the separation of light impurities from the exhaust air.

The initial section of the jalousie separator has a length $l_I$ and is horizontal, the final section has a length $l_{II}$ is vertical.

It is installed Г-shaped inertial jalousie-countercurrent dust collector with a height of inlet branch pipe $H_O = 0.16$ m, the angle of the jalousie grate $\alpha = 7^\circ$, the angle of the jalousie in the grate $\theta = 30^\circ$, a height of the outlet of the jalousie separator $h_J = 0.04$ m, a height of the outlet of the countercurrent separator $h_C = 0.04$ m, a length jalousie grate $L = 1.0$ m, the height of the camera for dust precipitation $H = 0.6$ m in the air system of seed cleaning machine that functioned on seed cleaning of barley variety Abava. The effect of the separating of light impurities from the exhaust air by the air system was an average value $E_O = 98.9\%$.

The developed methodology allows to determine the effect of light impurities separation from the exhaust air by the Г-shaped inertial jalousie-countercurrent dust collector quite accurately depending on its design parameters and fractional composition of grain dust particles.